Subject : Turbo Machines Unit No:1 Introduction to Turbo Machinery & Impulse Water Turbines

## **SYLLABUS**

## **Introduction to Turbo Machinery** (08 hrs)

Impulse momentum principle and its applications, Force excreted on fixed plate, moving flat plate and curved vanes, series of plates, velocity triangles and their analysis, work done equations , efficiency.

#### **Impulse Water Turbines**

Pelton wheel- construction, principle of working, velocity diagrams and analysis, design aspects, governing and performance characteristics, specific speed, selection of turbines, multi-jet.

## **Introduction To Turbo Machinery**

#### **Turbo machines:**

It is device that extracts energy from or imparts energy to a continuously moving stream of fluid (liquid or gas)

A turbo machine is a power or head generating machine which employs the dynamic action of a rotating element, the rotor; the action of the rotor changes the energy level of the continuously flowing fluid through the machine.

## **Impulse Momentum Principle**

When jet of water strikes on a flat plate or vane, it exerts a force in the direction of jet which is equal to rate of change in momentum in that direction.

Force= rate of change in momentum



 $F = \frac{mass}{time}$ (intial velocity - final velocty)

# Force exerted by the jet on stationery vertical plate

Let, V = Velocity of jet d = diameter of jet a = cross section area of jet



The Force exerted by the jet on stationery vertical plate in the direction of jet

F=rate of change of momentum in the direction of force

# Force exerted by the jet on stationery vertical plate



$$F = \frac{mass * initial velocity - mass * final velocity}{time}$$

$$F = \frac{mass}{time} [initial velocity - final velocity]$$

$$F = \rho a V (V - 0)$$
$$F = \rho a V^{2}$$

# Force exerted by the jet on stationery inclined flat plate



Mass of the water striking the plate=  $\rho aV$ Let,  $\Theta$  = angle between jet and plate V = Velocity of jet d = diameter of jet a = cross section area of jet

The Force exerted by the jet on inclined flat plate in the direction normal to the plate.

# Force exerted by the jet on stationery inclined flat plate

F=mass of the jet striking per second \*( (initial velocity of the jet in the direction normal to the plate- final velocity of jet after striking in the normal direction)  $F= \rho a V (V \sin \Theta - 0) = \rho a V^2 \sin \Theta$ 

This force can be resolved into two component. One in the direction of jet and other in the perpendicular direction of jet

The force in direction of jet,  $F_x = F X \cos (90-\Theta)$ 

 $= F \sin \Theta$ 

 $= \rho a V^2 \sin^2 \Theta \dots$ 

The force in normal direction of jet,  $F_y = F X \sin (90 - \Theta)$  $= F \cos \Theta$  $= \rho a V^2 \sin \Theta \cos \Theta....$ 

## Force exerted by a jet on a stationary curved plate



Component of velocity in the direction of  $jet = -v \cos \Theta$ 

Force exerted by a jet on a stationary curved plate

Force exerted by jet in the direction of jet,

Fx = ( mass / sec ) \*(initial velocity in the direction of jet – final velocity in the direction of jet)

$$Fx = \rho aV [V - (-V \cos \Theta)]$$
$$= \rho aV^2 [1 + \cos \Theta]$$

Force exerted by jet in the normal direction of jet,
Fy = ( mass / sec ) \* (initial velocity – final velocity in the normal direction of jet)

 $Fx = \rho aV [0 - V \sin \Theta]$  $= -\rho aV^2 \sin \Theta$ 

## Force exerted by the Jet on a curved plate at one end tangentially when the plate is symmetrical



Force exerted by the Jet on a curved plate at one end tangentially when the plate is symmetrical

Force exerted by jet in X direction
Fx = ( mass / sec ) \* (initial velocity in the direction of X – final velocity in the direction of X)

$$Fx = \rho a V [(V \cos\Theta - (-V \cos\Theta)]$$
  
=  $\rho a V [(V \cos\Theta + V \cos\Theta)]$   
=  $2\rho a V^2 \cos 2\Theta$ 

 $Fy = \rho a V [(V \sin \Theta - V \sin \Theta)]$ = 0

Force exerted by the Jet on a curved plate at one end tangentially when the plate is unsymmetrical



Let  $\Theta$  = angle made by the tangent at inlet  $\Phi$  = angle made by the tangent at outlet Force exerted by the Jet on a curved plate at one end tangentially when the plate is unsymmetrical

Fx = ( mass / sec ) \* (initial velocity in the direction of X - final velocity in the direction of X)

$$Fx = \rho a V [(V \cos\Theta - (-V \cos \Phi)]]$$
$$= \rho a V [(V \cos\Theta + V \cos \Phi)]$$
$$= \rho a V^2 (\cos\Theta + \cos \Phi)$$

 $Fy = \rho a V [(V \sin \Theta - V \sin \Phi)]$  $= \rho a V^2 (\sin \Theta - \sin \Phi)$ 

## Force exerted by a jet on a hinged plate



Force exerted by a jet on a hinged plate

X= distance if the centre if jet from hinge O  $\Theta$  = angle of swing about hinge W = weight o the plate acting at C.G. of the plate  $\Theta$ ' = angle between jet and plane

At equilibrium, two forces are acting on the plate, normal to the plate

1.force due to jet of water

 $Fn = \rho a V^2 \sin \Theta'$ 

2. Weight of the plate, W

Force exerted by a jet on a hinged plate

Moment of the Fn about hinge= Fn X OB=  $\rho aV^2 \sin \Theta' X OB$ =  $\rho aV^2 \sin (90-\Theta) X OB$ 

 $= \rho a V^{2} \cos \Theta X OB$  $= \rho a V^{2} \cos \Theta X \frac{\partial A}{\cos \theta}$  $= \rho a V^{2} X x$ 

Moment of weight w about hinge = W X OA' sin  $\Theta$ = W X xX sin  $\Theta$ 

For equilibrium of the plate,  $\sin \Theta = \frac{\rho a V 2}{W}$  W X x X sin  $\Theta = \rho a V^2 X x$ 

## Force exerted by a jet on a moving plate in the direction of jet



Force exerted by a jet on a moving plate in the direction of jet

Let, V = absolute velocity of the jet a = cross section area of the jet u = velocity of the flat plate

- Jet does not strike the plate with velocity V but with a relative velocity.
- Relative velocity of the jet with respect to plate = V- u Mass of the water striking the plate per sec =  $\rho a(V-u)$
- Force exerted by jet on the moving plate in the direction of jet = mass of water striking per sec X [ initial velocity with which water strikes- final velocity ]
- $= \rho a (V-u) [(V-u) 0]$
- $= \rho a (V-u)^2$

## Force exerted by a jet on a moving inclined plate in the direction of jet



Let,

- V = absolute velocity of the jet
- a = cross section area of the jet
- u = velocity of the flat plate
- $\Theta$  = angle between the plate and jet

## Force exerted by a jet on a moving inclined plate in the direction of jet

Relative velocity of the jet with respect to plate = V- u Mass of the water striking the plate per sec =  $\rho a(V-u)$ 

Force exerted by jet on the moving plate in the normal direction of plate = mass of water striking per sec X [ initial velocity with which water strikes in the direction normal to the plate- final velocity ] Fn =  $\rho a(V-u)[(V-u)\sin \Theta - 0]$ 

 $Fn = \rho a (V-u)^2 \sin \Theta$ 

 $Fx = Fn \sin\Theta = \rho a (V-u)^2 \sin \Theta \sin \Theta$  $Fx = \rho a (V-u)^2 \sin^2 \Theta$ 

 $Fy = \underline{Fn \cos}\Theta = \_\rho a (V-u)^2 \sin \Theta \cos \Theta$  $\underline{Fy} = \rho a (V-u)^2 \sin \Theta \cos \Theta$ 

## Force exerted by a jet on a moving curved plate in the direction of jet



Force exerted by a jet on a moving curved plate in the direction of jet

Component of velocity in the direction of  $jet = -(V-u) \cos\Theta$ Force exerted by jet in the direction of jet,

- Fx = (mass / sec) \* (initial velocity in the direction of jet final velocity in the direction of jet)
- $Fx = \rho a(V-u) [(V-u) (-V \cos \Theta)]$ 
  - =  $\rho a (V-u)^2 [1+\cos\Theta]$

Force exerted by jet in the normal direction of jet,

Fx = (mass / sec) \* (initial velocity in the normal direction)

- of jet final velocity in the normal direction of jet)
- $Fx = \rho a(V-u) [0 (V-u)sin\Theta)]$

= -  $\rho a (V-u)^2 \sin \Theta$ 



 $V_1$  = Velocity of the jet at inlet  $u_1$  = velocity of the vane at inlet  $Vr_1$  = relative velocity of the jet and plate at inlet  $\alpha$  = angle between the direction of the jet and direction of motion of the plate (Guide blade angle)  $\Theta$  = angle made by the relative velocity with direction of motion at the inlet (Vane angle at inlet)  $Vw_1$  = velocity of whirl at inlet ( component of  $V_1$  in the direction of motion)  $Vf_1$  = velocity of flow at inlet ( component of  $V_1$  in the direction perpendicular of motion)

## Similarly,

- $V_2$  = Velocity of the jet at outlet
- $u_2$  = velocity of the vane at outlet
- $Vr_2$  = relative velocity of the jet and plate at outlet
- $\beta$  = angle between the direction of the jet and direction

of motion of the plate (Guide blade angle)

 $\Phi$  = angle made by the relative velocity with direction

of motion at the outlet (Vane angle at outlet)

Vw<sub>2</sub> = velocity of whirl at outlet
( component of V2 in the direction of motion)
Vf<sub>2</sub> = velocity of flow at outlet
(component of V2 in the direction perpendicular of motion)

Inlet velocity Triangle:  $AC = V_1$ ,  $AB = u_1$ ,  $BC = Vr_1$ ,  $AD = Vw_1$ ,  $BD = Vf_1$ Outlet velocity triangle:  $GF = V_2$ ,  $EF = u_2$ ,  $EG = Vr_2$ ,  $FH = Vw_2$ ,  $GH = Vf_2$ As water glides smoothly , therefore neglecting friction between vane and water Vr1 = Vr2

Also tip velocity at inlet and outlet are same. u1 = u2

Force exerted by the jet in the direction of motion

= mass of water striking per sec X (initial velocity with which jet strikes the water in the dir. Of jet – final velocity in Direction of jet)

$$F = \rho a V r_1 [ (V w_1 - u_1) - (-u_2 + V w_2)]$$

$$=\rho a V r_1 [ (V w_1 - u_1 + u_2 + V w_2)]$$

 $F = \rho a V r_1 [V w_1 + V w_2]$ 

If  $\beta = 90^{\circ}$  then  $Vw_2=0$  .....F=  $\rho aVr_1 [Vw_1]$ 

If  $\beta > 90^{\circ}$  then  $Vw_2 = \dots F = \rho aVr_1 [Vw_1 - Vw_2]$ 

In general,  $F = \rho a V r_1 [V w_1 \pm V w_2]$ 

Work Done: Work done per sec by the jet = Force X Distance per sec W.D. = F X  $\frac{distance}{time}$ = F=paVr<sub>1</sub> [Vw<sub>1</sub>± Vw<sub>2</sub>] X u

Work Done : Work done per sec per unit weight of striking per sec = Force X Distance per sec / weight of water stinking per sec

$$F = \frac{\rho a V r_1 [V w_1 \pm V w_2] X u}{g X \rho a V r_1}$$

$$F = \frac{[Vw_1 \pm Vw_2]Xu}{gX} \cdots m$$

Efficiency :

It is a ratio of work done per sec to initial K.E. of Work done per sec per unit weight of striking per sec of jet

$$\eta = \frac{\rho a V r_1 [V w_1 \pm V w_2] X u}{\frac{1}{2} X m V_1^2}$$

Mass of water striking the vanes per sec=  $\rho a V_1$ 

moment of water striking in vanes in the tangential direction per sec at the inlet = mass of water X component of  $V_1 = \rho a V_1 X V w_1$ Similarly moment of water at outlet per sec =  $\rho a V_1 X (-V w_1)$ 

Angular momentum per second at inlet

= momentum at inlet X radius =  $\rho a V_1 X V w_1 X R_1$ 

Angular momentum per second at outlet

= momentum at inlet X radius =  $-\rho a V_1 X V w_2 X R_2$ 



Let, R1= radius of vane at the inlet of vane R1= radius of vane at the outlet of vane  $\omega$ = angular speed of the wheel  $u_1 = R_1 \omega$   $u_2 = R_2 \omega$ 

Torque exerted by the water on the runner, T = rate of change of angular momentum  $= (\rho a V_1 X V w_1 X R_1) - (-\rho a V_1 X V w_2 X R_2)$  $= (\rho a V_1) X (V w_1 X R_1 + V w_2 X R_2).....$ 

Work Done per sec = Torque X angular velocity =  $(\rho a V_1) X (Vw_1 X R_{1+}Vw_2 X R_2) x \omega$ =  $(\rho a V_1) X (Vw_1 X R_1 x \omega + Vw_2 X R_2 x \omega)$ W.D. =  $(\rho a V_1) X (Vw_1 X u_1 + Vw_2 X u_2)$ 

If angle  $\beta = 90^{\circ}$ , then W.D.= ( $\rho a V_1$ ) X ( $Vw_1 X u_1$ ) If angle  $\beta > 90^{\circ}$ , then W.D.= ( $\rho a V_1$ ) X ( $Vw_1 X - Vw_2 X u_2$ )

Efficiency of radial curve vane

$$\eta = \frac{\text{work done per sec ond}}{\text{kinetic energy per sec ond}}$$

$$\eta = \frac{\rho a v_1 [V w_1 u_1 \pm V w_2 u_2]}{\frac{1}{2} m V_1^2} \qquad \eta = \frac{2 [V w_1 u_1 \pm V w_2 u_2]}{V_1^2}$$

$$\eta = \frac{2 [V w_1 u_1 \pm V w_2 u_2]}{V_1^2}$$

Efficiency of radial curve vane Also W.D.per sec= change in K.E

 $\eta = \frac{change in kinetic energy per second}{kinetic energy per second}$ 

$$\eta = (1 - \frac{V_2^2}{V_1^2})$$

Hydraulic Machines: -Machine - Hydraulic Machine Types of Hydraulic Machines - Turbine (Converts Hydraulic energy into mechanical energy) - Pump (Converts mechanical energy into Hydraulic energy)

## Classification of Hydraulic Turbine

Depending upon energy available at the inlet of turbine
 Impulse

2. Reaction

2. According to the flow direction of flow through runner

- a. Tangetial flow
- b. Axial flow
- c. Radial flow
- d. Mixed flow

Classification of Hydraulic Turbine

3. Depending upon head available at the inlet of turbine

- 1. Low head T
- 2. High head T
- 3. Medium head T

4. According to the specific speed of the turbinea. Low specific speed turbineb. High specific speed turbinec. Medium specific speed turbine

Classification of Hydraulic Turbine 5. Depending upon position of shaft 1. Vertical shaft T 2. Horizontal shaft T

6. According to Name of Inventora. Pelton turbineb. Kaplan turbinec. Fransis turbine

## Impulse Water Turbines Pelton Wheel or Pelton Turbine

#### General Layout of hydraulic turbine



Pelton Wheel or Pelton Turbine

Construction and working of pelton wheel.



## Construction and working of pelton wheel

- 1. Nozzle and flow regulating arrangement
- 2. Runner and bucket
- 3. Casing
- 4. Breaking jet

## velocity Triangle for pelton wheel



## Velocity Triangle for of Pelton wheel

Let,

H= net head available at the inlet of the turbine D= diameter of the runner d= diameter of jet a = c/s area of jet N = speed of runner / wheel in RPM $V_1$  = Velocity of jet at inlet =  $\sqrt{2gH}$ Or  $V_1 = Cv_1/2gH$  Cv= Coefficient of velocity

Velocity of Blade=  $u_1 = u_2 = \frac{\pi dN}{60}$ 

## Velocity Triangle for of Pelton wheel

#### Inlet Triangle

Inlet triangle at inlet will be at straight line

$$Vr_1 = V_1 - u_1 = V_1 - u$$
  

$$Vw_1 = V_1$$
  

$$\alpha = 0, \ \Theta = 0$$

#### **Outlet Triangle**

As vane surface is smooth, neglecting friction
> Vr<sub>1</sub> = Vr<sub>2</sub>
> Vw<sub>2</sub> = Vr<sub>2</sub>cos Θ-u<sub>2</sub>

### Work Done for Pelton wheel

#### Force Exerted:

the Force exerted jet of water in direction of motion  $F = \rho a Vr_1 [Vw_1 + Vw_2]....$ for single vane  $F = \rho a V_1 [Vw_1 + \pm Vw_2]...$ for series of vane \*\* When  $\beta < 90^\circ$  then  $F = \rho a Vr_1 [Vw_1 + Vw_2]$   $\beta = 90^\circ$  then  $F = \rho a Vr_1 [Vw_1]$  $\beta > 90^\circ$  then  $F = \rho a Vr_1 [Vw_1 - Vw_2]$ 

#### Work Done:

Work done per sec by the jet = Force X Distance per sec W.D. =  $F X \frac{distance}{time}$ = $F=\rho a V_1 [Vw_1 \pm Vw_2] X u$ 

## Work Done for Pelton wheel

#### Work Done :

Work done per sec per unit weight of striking per sec = Force X Distance per sec / weight of water stinking per sec

#### Work Done:

Work done per sec by the jet = Force X Distance per sec W.D. = F X  $\frac{distance}{time}$ =F= $\rho a V_1 [Vw_1 \pm Vw_2] X u$ 

$$F = \frac{\rho a V_1 [Vw_1 \pm Vw_2] X u}{g X \rho a V_1} \qquad F = \frac{[Vw_1 \pm Vw_2] X u}{g} \cdots m$$

Efficiencies for Pelton wheel

(A) Hydraulic efficiency  $\eta h$  $\eta = \frac{work \, done \, per \, sec \, ond}{K.E.of \, jet \, per \, sec}$  $\eta = \frac{\text{work done per sec ond}}{K.E.of \text{ jet per sec}}$  $\eta = \frac{\sigma a V_1 [V w_1 + V w_2] X u}{\frac{1}{2} (\sigma a V_1) X V_1^2}$  $\eta = \frac{[Vw_1 + Vw_2]Xu}{V^2}$ 

<u>Maximum Hydraulic efficiency η</u> differentiating and equating it to zero. We get,  $u = \frac{V_1}{2}$ 

Efficiency of the Pelton wheel is maximum when the velocity of the wheel is the half the velocity of the

$$\eta_m = \frac{1 + \cos \varphi}{2}$$

<u>Maximum Hydraulic efficiency η</u> differentiating and equating it to zero. We get,  $u = \frac{V_1}{2}$ 

Efficiency of the Pelton wheel is maximum when the velocity of the wheel is the half the velocity of the

$$\eta_{max} = \frac{1 + \cos \varphi}{2}$$

<u>Hydraulic efficiency η</u>

$$\eta_{h} = \frac{runner \, power_{1}}{water \, power}$$

$$water \, power = \frac{\rho g Q H}{1000} kW$$

Water power

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water power = 
$$\frac{\rho g Q H}{1000} kW$$

Mechanical efficiency n

 $\eta_{m} = \frac{shaft \, power}{runner \, power}$ 

Volumetric efficiency

 $\eta_{vol} = \frac{volume \, of \, water \, actual \, striking \, the \, runner}{volume \, of \, water \, sup \, plied \, to \, the \, runner}$ 

Overall efficiency 
$$\eta_{o} = \frac{shaft power}{runner power} \times \frac{runner power}{water power}$$

$$\eta_{\circ} = \frac{shaft \, power}{water \, power} \times \frac{runner \, power}{runner \, power}$$

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$$\eta_o = \eta_h x \eta_m$$

## Design aspect of Pelton wheel

- 1. Velocity of jet V1=  $Cv\sqrt{2gH}Cv$ = coefficient of velocity
- 2. Velocity of Wheel  $u = \Phi \sqrt{2gH} \dots \Phi =$  speed ratio
- 3. The angle of deflection  $165^{\circ}$  (If not given) 4. Jet ratio m=(D/d)
- 5. Number of bucket Z= 15 + (D/2d)
- 6. Number of jet = ratio of total rate of flow through the turbine to rate of water through single jet

## Performance of Pelton wheel

Turbines are designed to work under a given head ,discharge and output. To check performance of turbine under different working condition following parameters are observed.

- 1. Speed
- 2. Head
- 3. Discharge
- 4. Power
- 5. Overall efficiency

By keeping one independent parameter constant, variation of the parameters are plotted.

These curves are called characteristic curve.

## Characteristic Curve

- 1. Main characteristic curve or constant head curve
- 2. Operating characteristic curve or constant speed curve
- 3. constant efficiency curve

Main characteristic curve or constant head curve



## Characteristic Curve

1. Operating characteristic curve or constant speed curve



## Characteristic Curve

Constant efficiency curve



Governing of Pelton wheel Process by which speed of the turbine is kept constant at all operating condition

Oil pressure governor



## Specific speed of Pelton wheel

It is speed of turbine which is identical in shape ,geometrical dimension ,blade angle with the actual turbine But of small size so it will develop unit power working under unit head

$$N_{s} = \frac{N\sqrt{P}}{H^{\frac{5}{4}}}$$

#### Application of specific speed

Sr. No,	Specific speed in MKS	Specifc speed in Sl	Type of Turbine
1	10-35	8.5-30	Pelton wheel with single jet
2	35-60	30-51	Pelton wheel with two jet
3	60-300	51-225	Fransis turbine
4	00-1000	225-860	Kaplan turbine

## Solved Numerical

Q.1A Pelton wheel has a mean bucket speed of 10 m/sec with jet of water flowing at the rate of 700 lit /s under a head of 30 meters. The buckets deflects the jet trough an angle of 160<sup>0</sup>. Calculate the power given by water to the runner and the hydraulic efficiency of the turbine. Assume coefficient of velocity as 0.98

Given Data:Speed of the bucket,  $u_1=u_2=u=10$  m/s Discharge Q= 700 lit /s m<sup>3</sup> /s Head of the water H=30 m Angle of deflection =160 Angle  $\Phi = 180-160=20^{\circ}$ coefficient of velocity = 0.98

## Solution

the velocity of the jet =  $V_1 = Cv\sqrt{2gh} = 23.77$  m/s

 $Vr_1 = V_1 - u_1 = 23.77 - 10 = 13.77 m/s$  $Vw_1 = V_1 = 23.77 m/s$ 



From outlet velocity triangle  $Vr_1 = Vr_2 = 13.77 \text{ m/s}$   $Vw_2 = -Vr2\cos\Phi - u_2$ =13.77 cos 20<sup>0</sup>-10 =2.94 m/s

## Solution

#### W.D./sec

- W.D./sec =  $\rho a V_1 (V w_1 + V w_2) X u$ =1000 \*0.7\*[23.77+2.94] \*10
- $=1000 \times 0.7 \times [23.77 + 2.92]$ =186970 Nm /s



Power Given to the turbine, P = 186970 /1000 = 186.97 kW

The hydraulic efficiency of the turbine given by the equatio  $\eta_h = 2 [vw1 = vw2] * u / V_1^2$ 

=0.9454=94.54%

## Solved Numerical-2

Q. Two jets strikes the bucket of pelton wheel which having shaft power as 15450 KW. The diameter of each jet is given as 200 m. if the net head at the turbine is 400 m, find the overall efficiency of the turbine. Take Cv = 1.

Given Number of jet =2 Shaft power = p = 15450 KWDiameter of jet= d= 200 mm = 0.20 mArea of the jet =a = 0.31416 m2Net head = H= 400m Cv =1

## Solution

Velocity of the jet =  $V_1 = Cv\sqrt{2gh}$ = 1  $\sqrt{2 * 9.81 * 400}$ = 88.58 m/s

discharge of each jet = $q = a * V_1 = 2.78 m^2$ 

Total discharges

= Q = 2 \* 2.78

 $= 5.56 \text{ m}^3/\text{s}$ 

Power at the inlet of the turbine , WP=  $\rho g Q H /1000 kW$ =1000\*9.81\* 5.56\*400/1000 = 21817.44 kW

Overall efficiency is given as =  $\eta_0 = SP/WP$ =15450/21817.44 = 70.8

